

Establishing links between performance-based durability design and sustainability

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Presentation overview

Contents

Durability design/specification (with an eye on sustainability) :

- Prescriptive approach
- Performance-based approach
 - Deemed-to-satisfy approach
 - Full- probabilistic approach
 - Comparison of results

Links between durability and sustainability

Introduction

Prescriptive specifications do not adequately address sustainability issues

- ☐ Do not have the flexibility in addressing new or marginal materials
- ☐ Conservative approach – may result in resource waste
- ☐ Danger of under-specification for severe environments leading to premature failure
- ☐ No means to check actual specification requirements, in particular the as-built quality

Introduction

Consequences:

- The resulting concrete is 'indeterminate' (in the sense that we do not really know what we have got)
- It may actually be inadequate to the task, thus requiring repair and maintenance during the structure's service life resulting in:
 - Unanticipated material consumption
 - Social disruptions

Introduction

- On the other hand, it may be over-conservative
- The irony is that, while many current durability specifications are viewed as being over-conservative, we have the phenomenon of a massive stock of under-performing infrastructure in respect of longevity and durability
- This is simply 'un-sustainable'

Performance-based Durability Design and Specification

Performance-based design

Performance-based design and specifications limit the environmental consequences on the structure to defined acceptable levels (targets) during the structure's service life (e.g. a pre-defined level of deterioration or state of repair)

Performance-based design

General framework for performance-based design:

1. A Robust Quality Control Test (or Tests)

Routine, easily-carried out, reliable measures of resistance to deterioration (e.g. to chloride ingress)

2. A Service Life Model

This must relate performance to the quality control test (e.g. in terms of limiting material parameters)

3. Able to account for Differences (i.e. 'Margins') between 'Material Potential' and 'As-Built' Values

In order to differentiate between areas of responsibility (e.g. material supplier & constructor)

Next section illustrates the above with reference to SA developments

Performance-based design

1) Quality control tests:

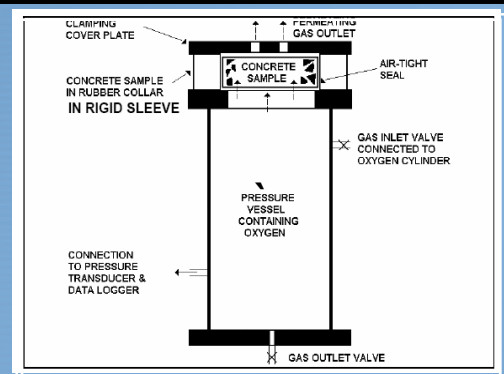
– the approach developed in SA is that of *durability index (DI) tests* which serve as practical tools for durability studies, and to characterize the resistance of concrete to ionic or molecular transport



1. Chloride conductivity



2. Water sorptivity



3. Oxygen permeability

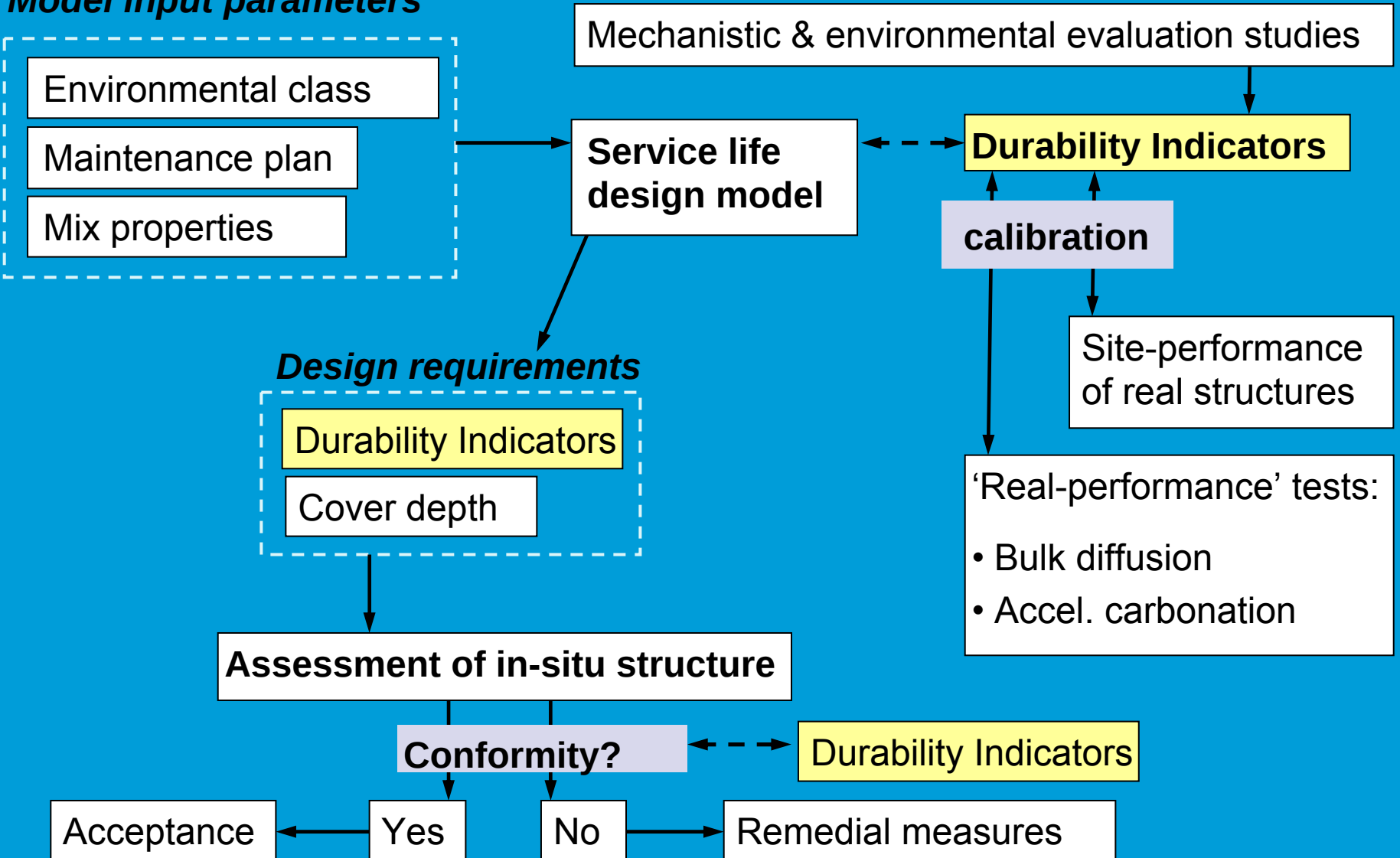
Performance-based design

2) Service-life models

- One SLM for chloride resistance, using 28-day chloride conductivity as an input to a Fickian-type model
- One SLM for carbonation resistance, using 28-day OPI as a parameter - empirical
- Initiation models - Account for material type and environment
- Link between DI parameters & use in SLM – integrated approach

Integrated Design Framework & Methodology

Model input parameters

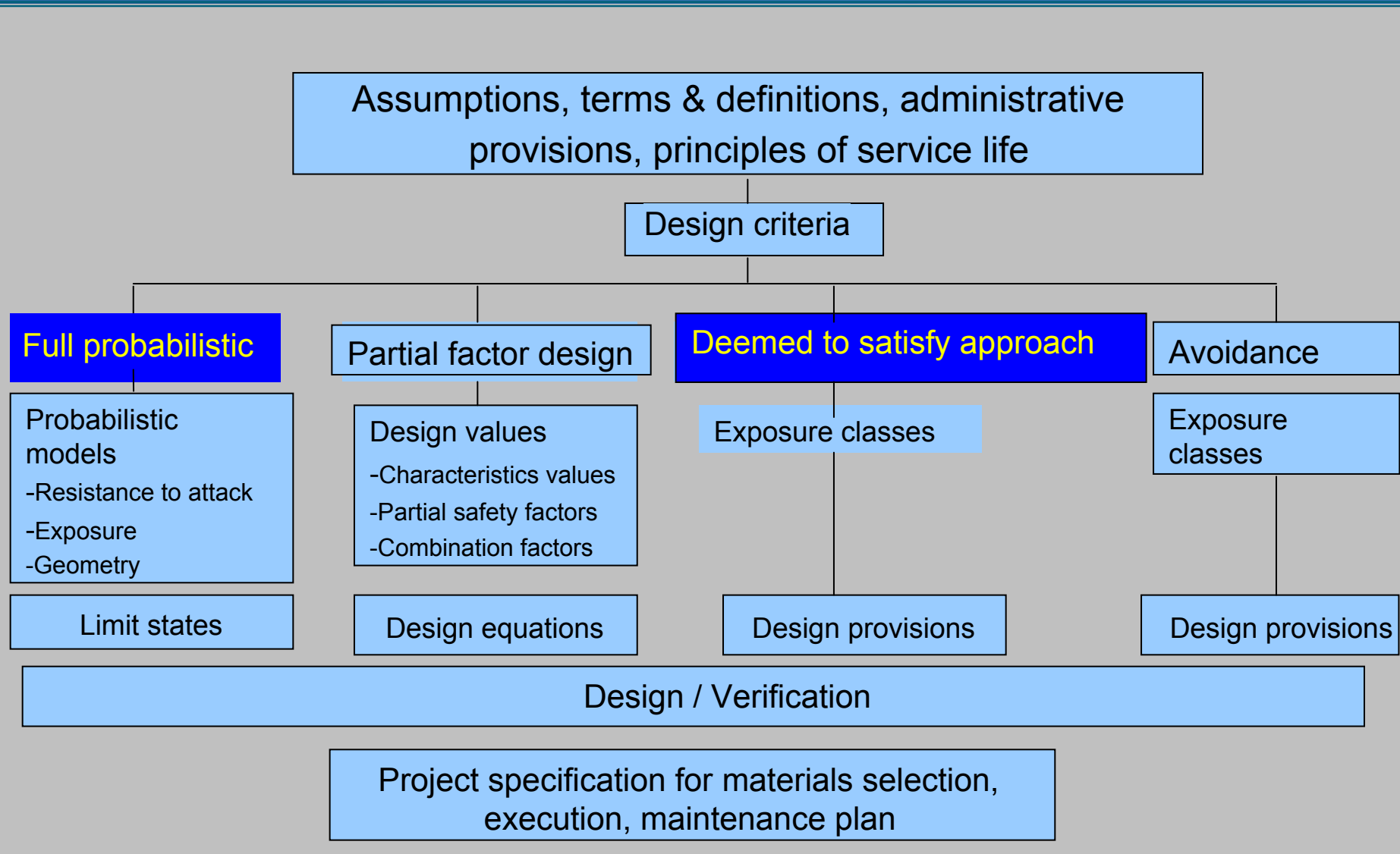


Performance-based design

Design methodology has been applied to two conditions (ref FIB Model Code):

- Deemed-to-satisfy approach
- Full- probabilistic approach

fib Model Code Framework



1) Deemed-to-satisfy approach

1. Performance criteria are drawn from the relevant SLM
2. The emphasis is on as-built concrete quality
3. Characteristic values of design parameters are used
4. Margin allowed between material 'potential' and as-built quality

Cont... I) Deemed-to-satisfy approach

1. Performance criteria are drawn from the relevant service-life model

$$C_x = C_s \left(1 - \operatorname{erf} \left(\frac{x}{2\sqrt{D_c t}} \right) \right)$$

C_x = chloride concentration at depth x and time t

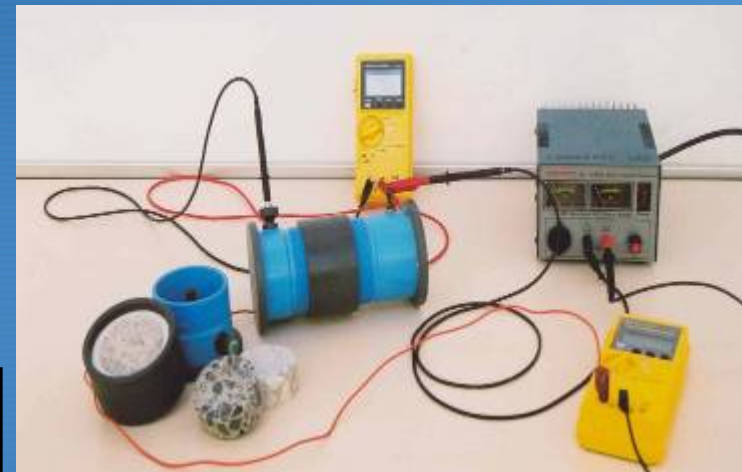
C_s = chloride surface concentration

erf = mathematical error function

D_c = diffusion coefficient

CC values: from < 0.5 to 3.5 mS/cm

$$\sigma = \frac{i \cdot t}{V \cdot A}$$



Cont... I) Deemed-to-satisfy approach

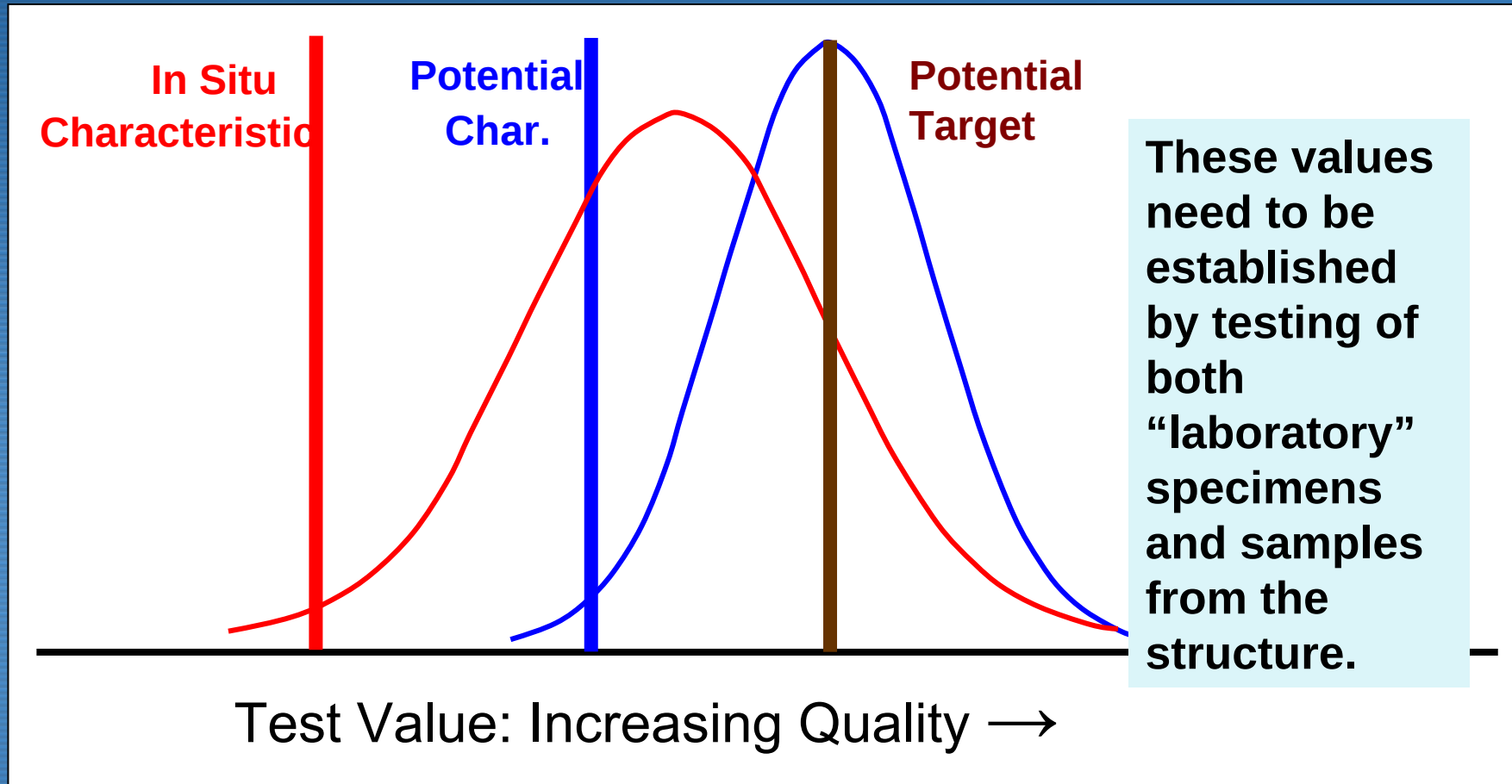
Example of performance criteria – CC values

Table 1: Example: chloride-conductivity, 100 y life

Marine Structure 50-yr design life		Max. chloride conductivity (mS/cm) for various binder types		
		100% CEM I	30% fly ash	50% Corex slag
Exposure class (based on EN 206)	Cover (mm)			
XS3b: Tidal, splash and wetted spray zones, exposed to abrasion	40	0.45	0.75	1.05
	60	0.95	1.35	1.95
	80	1.30	1.80	2.60

Material Potential vs As-Built Values

2.-4. As-built quality; Char. Values; Margins allowed



II) Full-probabilistic Approach

- The methodology for a full-probabilistic design follows limit-state format given in ISO 13823 – which groups the design variables into either load (S) or resistance variables (R)
- Each variable is represented as a stochastic quantity

$$g(x, C_{\text{crit}}, C_s, D_c, t, m) = R - S = 0$$

II) Full-probabilistic Approach

The design objective is to ensure that the calculated P_f for a given set of parameters does not exceed a target P_f given in the standards for a defined limit state

$$P_f = P\{R - S < 0\} < P_{\text{target}}$$

and for the initiation limit state (ILS):

$$P_f = P\{C_{\text{crit}} - C_{(x,t)} < 0\} < P_{\text{target, ILS}}$$

where

$$C_{(x,t)} = C_s \left(1 - \text{erf} \left(\frac{x}{2\sqrt{D_i t^{(1-m)}}} \right) \right)$$

Solution of the LSF is carried out using Monte Carlo Simulation techniques that give the probability of failure

Design Example



Design Example

Use careful probabilistic assessment to give a realistic probability of failure and an air resistance to (XCB) and integrity threat should be specified in design and ground granulated blast furnace slag (GGBS)

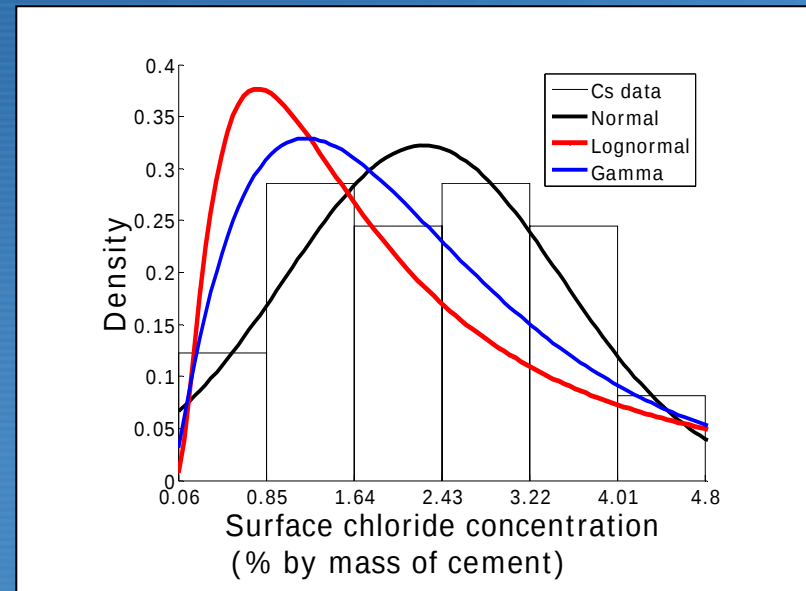
Design life = 100 years



Design Example: Probabilistic approach

Statistical quantification of parameters in the LSF is carried out by fitting distribution curves to data obtained from in-situ testing. e.g. for C_s from profiling tests on existing RC structures (3-75 yrs) in SA

$$g(x, C_{\text{crit}}, C_s, D_c, t, m) = R - S = 0$$



Design Example: Probabilistic approach

Using the statistical quantities for each parameter, a MCS of the LSF is done to get an output represented by a cumulative density function (CDF)

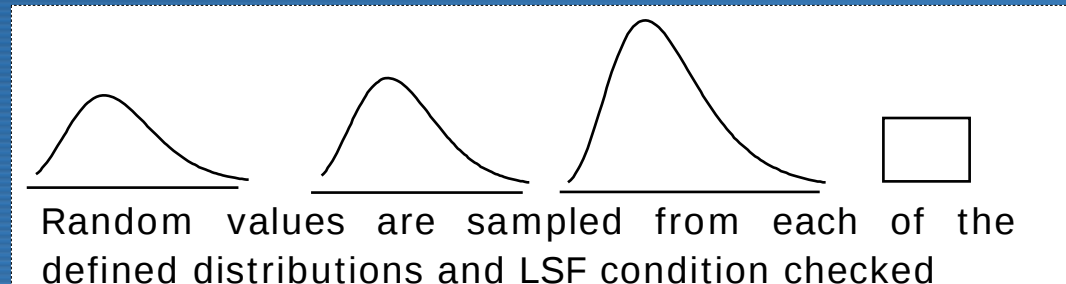
Table 2: Input parameters for reliability analysis of RC Pier

<i>Parameter</i>	<i>Units</i>	<i>Mean</i>	<i>COV[#]</i>	<i>Distribution</i>
x	mm	50	0.2	Normal
C _{crit}	%	0.48	0.31	Normal
C _s	%	4.13	0.21	Gamma
t	years	100	-	Deterministic
m	-	0.68	-	Deterministic

COV[#] = Coefficient of variation

Design Example: Probabilistic approach

MCS carried out using a Matlab sub-routine



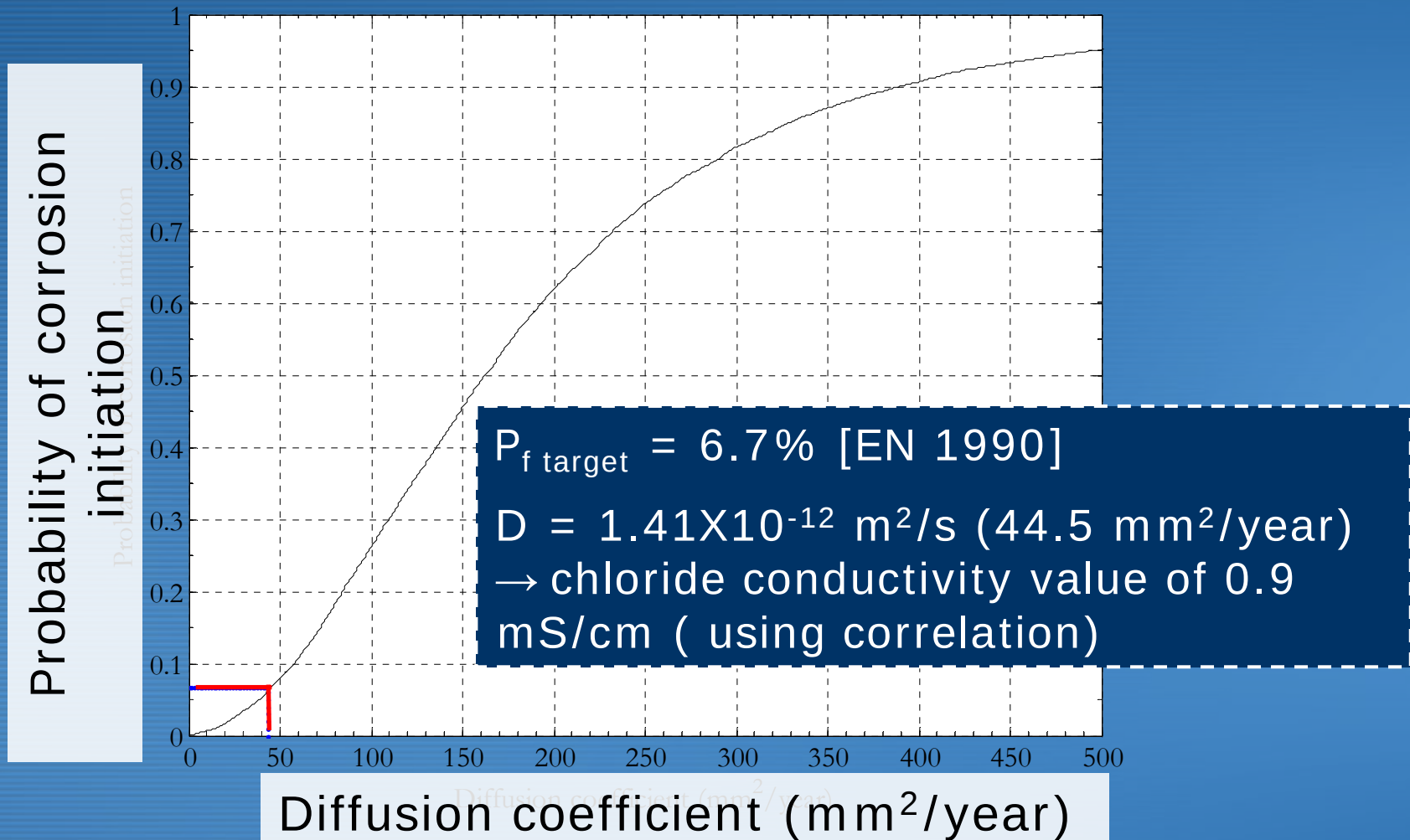
Process is repeated a number of times
(10 000 iterations = N)

If for a set of random values sampled $LHS < 0$ then failure is said to occur & program registers this event (n)

P_f is then computed as:

$$P_f = \frac{n}{N}$$

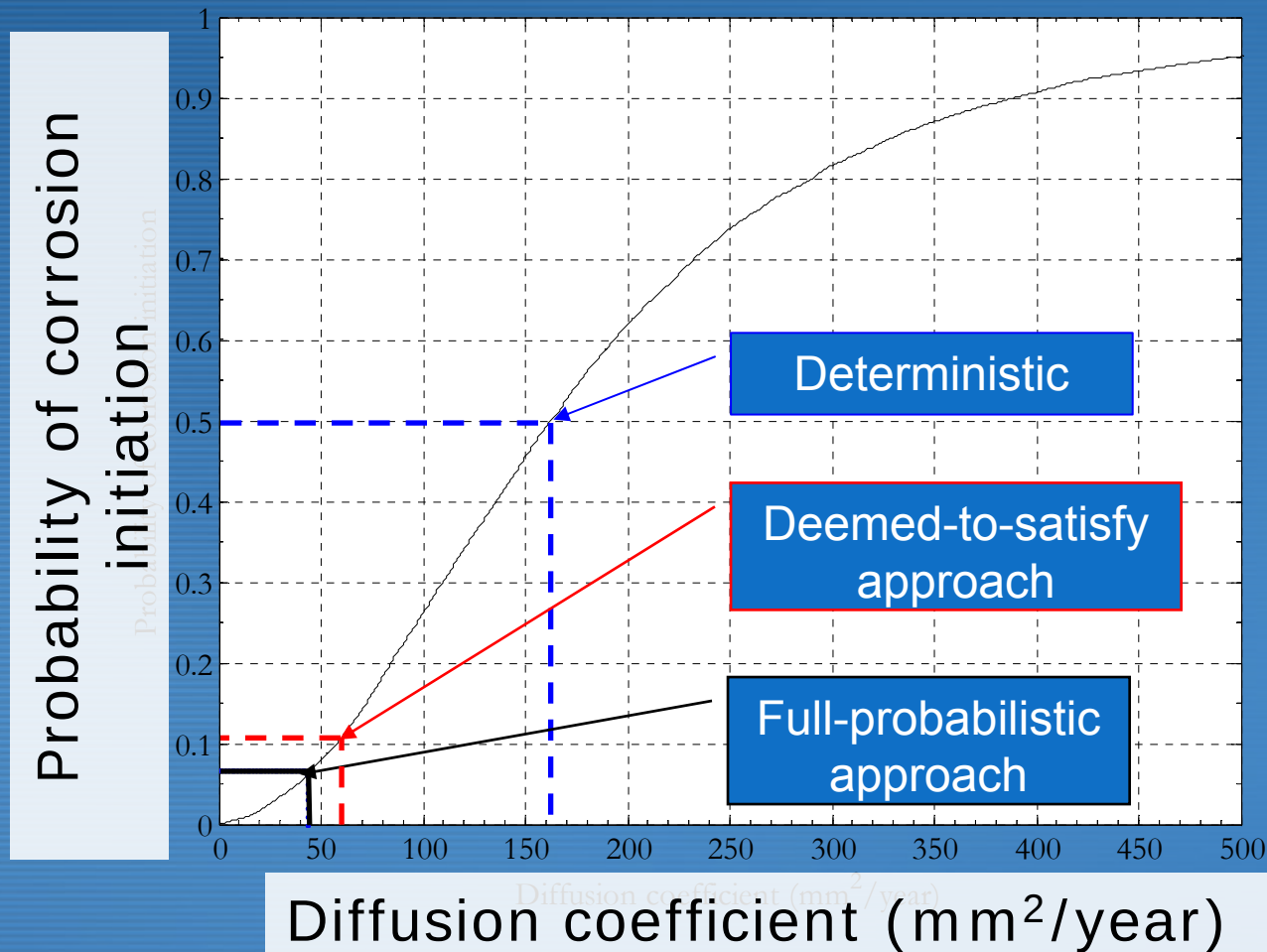
Design Example: Probabilistic approach



II) Probabilistic Approach

- The probabilistic approach provides a means to deal with the variability in durability design parameters
- The approach gives a more realistic representative of the 'real life' situation where variability is inherent, as compared to the deemed to satisfy or deterministic models

Deemed-to-satisfy vs Full Probabilistic



Performance-based approach

It can be argued that a purely deterministic approach should give a CC equivalent to 50% P_f

Table 3: Design specifications (XS3b; Cover = 50mm $\pm \Delta x_{dev}$; CEM III A)

<i>Design method</i>	<i>Chloride conductivity value</i>
Deterministic (50% P_f)	1.92 mS/cm
Deemed-to-satisfy (DTS)	1.05 mS/cm
Full-probabilistic (6.7% P_f)	0.9 mS/cm

Performance-based approach vs Prescriptive Approach

For the example, the table below compares three approaches to durability design

Table 4: Design specifications (XS3b; Cover = 50mm $\pm \Delta x_{dev}$; CEM III A)

<i>Design method</i>	<i>Quality control test value e.g. CC (CEM IIIA)</i>	<i>water/ binder</i>	
		<i>CEM IIIA</i>	<i>CEM I (Equiv.)</i>
Prescriptive approach (EN 1992-1-1:2004)	-	0.4	-
Deemed-to-satisfy	1.05 mS/cm	0.75 [#] /0.55	0.30
Full-probabilistic	0.9 mS/cm	0.70 [#] /0.55	0.25

= due to limitations in the current state of knowledge, a maximum w/b=0.55 is recommended

Summary of Performance-based approach:

- Quantification of the problem,
- Idea of design 'targets', and
- A design framework for engineers

Links between sustainability and durability

Links between sustainability and durability

Durability design and Sustainability:

- ❑ Inadequate durability leads to need for repair and rehabilitation - unnecessary waste of resources
- ❑ Should allow efficient use of resources
- ❑ Should allow utilization of new materials

BUT: how can we use the concepts of durability design to assist us to develop 'sustainability design'

Links between sustainability and durability

- So far structural reliability theory has provided a *quantitative link* between the practice of structural engineering and its economic and societal consequences – mainly struc. safety

Table 5: Consequences classes for SLS (FIB Model Code)

<i>Consequences class*</i>	<i>Reliability level</i>	<i>Probability of failure (P_{target})</i>
CC1 (Low)	1.0	16%
CC2 (Normal)	1.5	6.7%
CC3 (High)	2.0	2.3%

*The reliability level is selected based on consequences of failure i.e. If there will be many lives lost (public building) then a higher reliability level is selected

Links between sustainability and durability

- The target prob. of failure (P_{target}) values are derived from optimizing the direct economic benefits/costs incurred by the owner/manager of the infrastructure.
- If the calculated P_f departs from P_{target} then the design is deemed uneconomical
- The P_{target} values at this stage relate to design standards established by developed countries; these may not relate to economic conditions faced in developing countries, e.g.
 - quality control levels might have to differ
 - 'development' may be more important than resource minimisation

Links between sustainability and durability

- At present, the P_{target} value does not assign a value to the loss suffered by the society (user) when durability/structural failure occurs E.g. loss due to:
 - Inconvenience during repair
 - Loss of assets in case of structural failure
 - Loss of income due to repair
 - Possible loss of life

Links between sustainability and durability

- Likewise, the environmental consequences are equally important but so far have not been included in the analysis of P_{target} (or an equivalent formulation)
- Environmental consequences of durability failure may include:
 - Consumption of additional energy and resources due to repair
 - Generation of wastes during repair
 - Loss of the original materials

Links between sustainability and durability

- We need to go a step further and estimate (using actual values) the societal and environmental consequences i.e. the explicit impact of durability/structural failure related to a particular target reliability
- These might vary from country to country depending on the state of development

Links between sustainability and durability

Previous cost minimization function:

$$Z(p) = C(p) + [F \times P_f]$$

P = design criteria

C(p) = Design and construction cost

F = Direct material losses due to failure

Proposed cost minimization function:

$$Z(p) = C(p) + [(F + S + E) \times P_f]$$

S = Societal cost due to failure

E = Environmental cost

Concluding comments

- To summarise: we have argued that considerations of sustainability should relate to concepts embedded in service life and performance-based design requirements of structures
- This would in turn allow for the comparison of different material design options on the basis of their performance, as opposed to the current practice of comparing their costs and/or environmental impacts without a common reference of performance
- Introduction of such a system will lead to the promotion of new environmentally friendly structures that meet economic and societal needs

Thank You

